

③ Two wiring systems that would be suitable to be used as unprotected supply conductors originating at terminal of stand by generator.

Wiring system with WS classification (7.2.2.2.1) when WS classification is not specified

(7.2.2.2) - The wiring system shall be of a type that

- (a) capable of maintaining supply to the equipment when exposed to fire either fire (or) mechanical damage (or)
- (b) capable of maintaining supply to the equipment when exposed to fire and protected against mechanical damage by (a) installing suitable enclosure (or)
- (c) installation in a location where the system will not be exposed to mech damage.

④ Maximum permissible unprotected cable length

B.6.13.1 - Table 8.3 max. cable length. S.S.3 4.12.5.1 - 150m
NSW Electrical Service Rule 7.3.5.1

⑤ use of stand by generator.

7.3.3 control 7.3.4.2 7.3.5

shall be controlled by main switch

7.3.4. Isolation, 7.3.4.2 Isolation of batteries

7.3.5 provided with over current protection.

⑥ ~~As 3010~~ - At least one door (3.2.3.2) - 3 months

⑦ checking - Exhaust system (manifold, muffler, pipes)

⑧ Fuel system (supplies, return lines, filters)

⑨ Ignition system (batteries, chargers)

⑩ Engine (fluid level, oil pressure, coolant temperature filters, radiator hoses, belts, bearings, fitting guards)

⑪ ventilation equipment

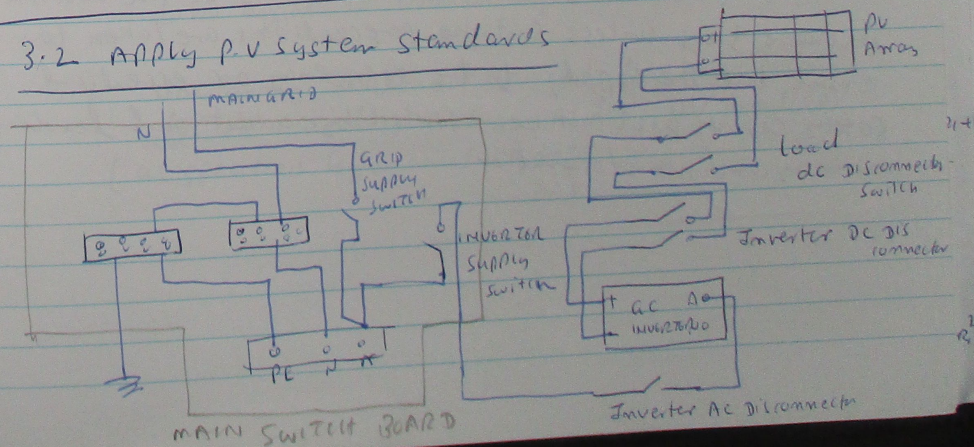
⑫ control / protection settings

⑬ Testing

6-12 months

- sample test for oils for particles and chemical composition
- functionality of change over switch (check)
- Test operation parameters under simulated emergency condition
- check functionality of alarms and indicators

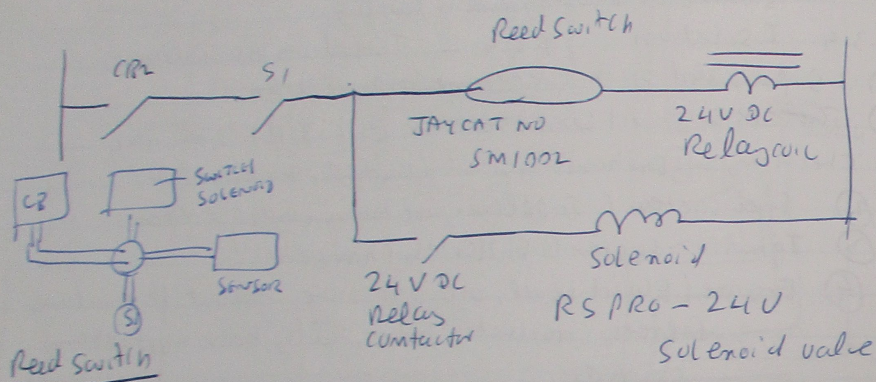
3.2 Apply P.V system standards



<https://www.jaycar.com.au/complements-electromechanical/switches/>

* JAYCAR - CAT NO (SM1002) - miniature glass Reed Switch

* RS - STOCK NO (784-002) RS PRO 24V Solenoid valve



It is closed on presence of magnetic field. It is also a sensor.

2.2 @ 5 AS 3010 / 3.6.5

Supply of other than emergency system (or) essential services
A single generating set shall not be used for purpose other than the supply of emergency or essential safety service described in clause 3.6.1 unless suitable precautions are taken to ensure that the supply to the emergency or essential safety services will not be affected by additional loading under any condition of operation.

reed-switch/c/201

3-2 1/ The requirement for protection of cables running ~~not~~ between the array and inverter of a grid connected PV system.

AS 503 / 2-4-5 PV array cables of the system connected to batteries shall be protected with fault current protection devices

2) Requirement for PV system cabling

AS 5033 / 3-5 - where PV array cabling could be confused with other wiring systems, appropriate identification shall be provided at regular intervals. Typically identification shall not be more than 3m apart.

3) minimum IP rating for grid connected PV system components installed outdoors.

4-2-1 PV array and PV sub array junction box exposed to the environment shall be at least IP54 compliant in accordance with AS 60529 and shall be UV resistant.

4) maximum Array voltage for domestic grid connected PV system

AS 5033 / 4-2-8 - The PV array voltage shall be considered to be equal to $V_{oc\ array}$.

3.2 $V_{oc\ array}$ shall not exceed the maximum allowed operating voltage of the PV modules (as specified by manufacturer)

4.3 Inspect battery systems

- Hazards
Battery Acid | D/H use safety glass for eye protection
hurts eye
Battery acid injury on hand | D/H use appropriate safety glove
Acidic fumes | D/H use battery room ventilation
inhale
Location ETC college Type - solar Electrical system

① Environmental condition

- 4.1 Area in which the battery is installed is suitable (Y)
ventilated
1.2 Ambient temperature and humidity are suitable for the battery system (Y)
1.3 NO external heat source are present that may cause hazardous temperature rise (Y)
1.4 Access and egress from the area is unobstructed (Y)

② Battery system (Items)

- 2.1 System shut down and start up procedures documented and available (Y)
2.2 All required signs, labelling and markings are installed (As per AS/NZS 5139 section 7) (Y)
2.3 Shut down and start up procedures are consistent with diagrams and labelling (Y)
2.4 All required isolation devices are installed and are operating correctly. (Y)
2.5 All terminations are suitably tight (Y)

- 2.6 All required controls are installed correctly (Y)
2.7 All required protection devices and enclosures are installed correctly (Y)
2.8 All required monitoring and alarms are installed correctly (Y)
2.9 All battery system equipment is free from damage (Y)
2.10 All battery system equipment is free from excessive dust, dirt and debris (Y)

③ System Parameters - Items

- 3.1 Battery charger settings are suitable for the equipment and desired functionality (Y)
3.2 Inverter settings are suitable for the equipment and desired functionality (Y)

- Q1 Two types of batteries commonly used in backup (emergency battery bank)
- Lithium Ion battery
- Lead acid battery

- Q2 How many 6V, 100Ah, VRLA batteries are required to produce a battery bank with a rated o/p 120V, 200AH

$$\begin{array}{l} \text{|||} - \frac{120V}{100\text{Ah}} \text{|||} \xrightarrow{6 \times 20 = 120V} \\ \text{|||} - \frac{120V}{100\text{Ah}} \text{|||} \xrightarrow{6 \times 20 = 120V} \end{array} \quad \begin{array}{l} 40 \\ 40 \end{array}$$

$100\text{Ah} + 100\text{Ah} = 200\text{Ah}$

- Q3 Minimum spaced requires between 2 batteries (side by side)
600mm { AS/NZS 5139:2019 400

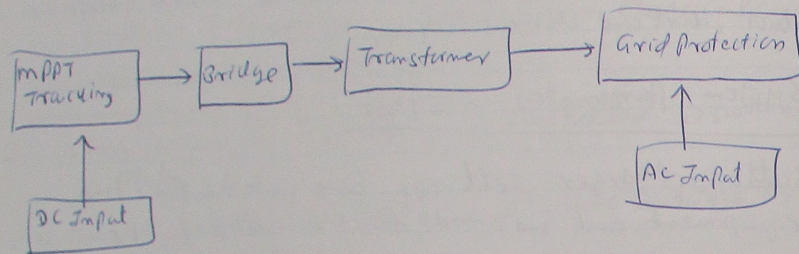
- Q4 Minimum vertical clear clearance between tiered batteries
900mm { AS/NZS 5139:2019 400

5.2 Draw Inverter Symbols and Diagrams

2.1 Australian Standard Symbol for L.V. Separated Inverter



2.2 Grid connected Inverter block diagram



3 Functions of Inverter in Grid connected system

- 1/ Central Inverter - string Inverter (connected to entire PV array)
- 2/ multimode Inverter - Allow for islanding (The installation can continue to operate from the alternate supply in the event of main failure) (Trigger grid protection to disconnect the alternate supply)
- 3/ micro Inverters - (designed to use with PV arrays, consists of several small inverters each connected to individual modules within the array, typically mounted on to array assembly)

6.1 ALternative Supply Risk Assessment

Source 1	240V AC Grid power	Location	ETC workshop
Source 2	Solar Electrical system	Location	PV Room

Type of Hazard

High voltage	✓ worked height	✓ foreign bodies	Explosive
✓ Low voltage	Hot work	asbestos	90,
✓ Extra Low voltage	confined space	✓ dust	Toxic gas
High current	UV radiation	✓ noise	Explosive
✓ working live	mobile plant/dredging	✓ manual handling	chemical
✓ House keeping	✓ power tools		corrosive chemical
✓ other		mechanical handling	Toxic chemical
			Flammable

Tasks

240V Grid

- 1) Isolate the main supply, identify the point of supply
- 2) switch off the isolator
- 3) Perform maintenance tasks
- 4) Inspect the insulation resistance of wiring system
- 5) Inspect and secure the connections

PV

- 6) Install / connect PV panel
- 7) Perform solar array wiring and connections
 - 1) connect PV modules and arrays
 - 2) PV module protection
 - 3) DC/AC Isolator installation
 - 4) Install and operate inverter

SEVERITY	LIKELY	POSSIBLE	UNLIKELY	
Death or permanent disability	1	1	2	1/ extreme risk 2/ High Risk 3/ medium risk
Serious injury or chronic illness	1	2	3	4/ Low Risk
Minor injury, require first aid	2	3	4	

Task	Job steps	Potential Hazard	Associated	Risk	Risk Level	Control measure	Responsible
1	240V Exposed conductor	Electrocution	Barrel out	of equipment	1	Test terminal / Enclose	Person Supervisor
2	Faulty Isolator	Dangerous voltage presence	Wrong	energizing	2	Test isolator without Live	Supervisor
3	untagged / unlabeled main switch	Electrocution	Injury	Equipment damage	1	properly perform Locking Tagging	Supervisor
4	Insulation Resistance Failure	L-L fault L-N fault Live Earth	Electrocution		3	Perform before Test before energizing	Supervisor
5	Reverse polarity N-E	Electrical Leakage to Earth.	Electrocution		3	Perform polarity Test	Supervisor
6	Falling from height	Injury	Equipment	damage	1	use appropriate fall protection equipment	Supervisor
7	Insulation failure of connection wires	Electrical Faults	module / system	Damage	2	use correct size wire protection	Supervisor
8	safety diode failure	pu module reverse charge	module over	heating damage	4	use correct rating diode	Supervisor
9	Too appropriate sized isolator	Isolator switch damaged	Electrical shock	leakage	4	use appropriate size isolator	Supervisor
10	Batteries Installation	Batteries terminal Faults	Batteries over	charge	4	Properly tighten batteries terminal connection	Supervisor
11	Inverter installation	Faulty Inverter	out put	frequency	4	Test the inverter before use	Supervisor

Shutdown procedure

- ① Identify the point of supply and affected systems
- ② Identify all isolation switches
- ③ measure voltage, frequency before switching off
- ④ Isolate the supply
- ⑤ measure the affected points
- ⑥ set all equipment at off positions
- ⑦ Locking and Tagging

S-3 connect and Test an Inverter

Hazards

- Falling from height \Rightarrow H use fall protection gear
- pulling short circuit \Rightarrow H Test insulation resistance
- output circuit electrical short circuit \Rightarrow H Test insulation resistance.
- Battery acid injury \Rightarrow H use glove eye protection
- Exposed terminal \Rightarrow H enclose the exposed terminal.

Inverter Specification

DC Input

max. input power = 670 watt
 max. input voltage = 60V
 MPPT voltage range 90 - 560V

max. input current = 25A
 max. No. of strings 14

AC output

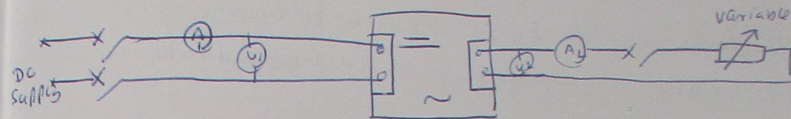
nominal output power = 300W
 max. output power = 330Watt
 Nominal ac voltage range 180/270V

max. output current = 9.11 - 9.62A
 Frequency Range 45-55/55-65Hz

Characteristics

maximum efficiency 85.8%
 Temperature range $-25 \sim +60^{\circ}\text{C}$
 power factor 0.82

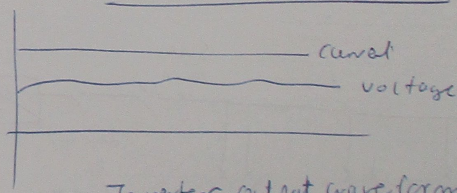
connect the inverter to dc supply and variable ac load as shown below



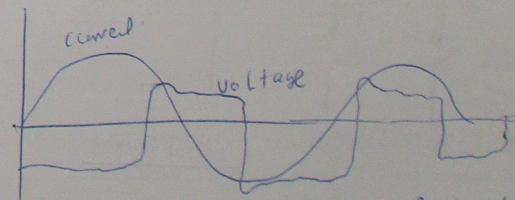
View Inverter testing video and data sheet

LOAD	Inverter operating characteristics				
	dc Input voltage V	dc Input current A	AC output voltage V	AC output current A	Efficiency %
No Load	22V	4A	28V	0	0
Load 1	22	4	27	3	92%
Load 2	22	4	23.8	3.5	95%
Load 3	22	4	22.2	3.7	96%

Inverter Input wave form



Inverter output wave form



Grid connected Inverter Passive Protection

- ① Passive Protection method monitors the voltage and frequency variations. When one or more of these parameters deviate from the permitted threshold range, an islanding event is considered to have occurred and relay circuit removes the inverter from the supply.

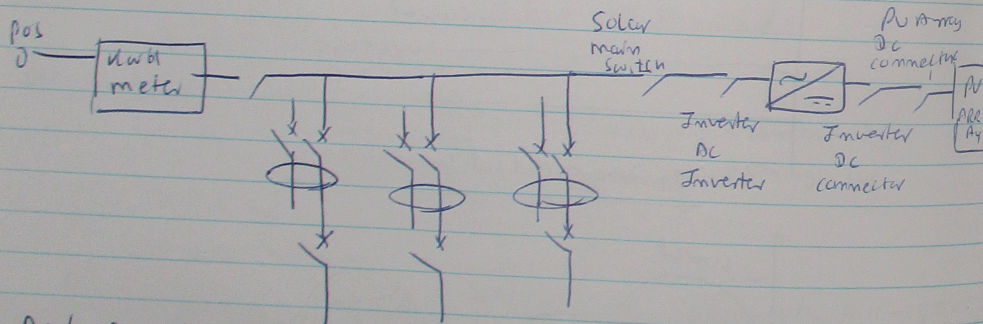
Grid connected Inverter Active Protection

- (2) Active methods generate the perturbation to change grid parameters such as magnitude of grid voltage and frequency in the allowable range. Slip mode frequency shift is utilized. This varies the reactive power output of inverter. The goal of this protection method is to destabilize an islanded feeder by trying to influence the frequency.

MPPT Algorithm

- (3) MPPT is the algorithm that included in charge controllers used for extracting maximum available power from PV module under certain conditions. It calculates the best amount of power that the panel can provide to charge the battery.

6.2 Shutdown, Isolate and Restart an Alternating Supply System



SHUT DOWN

AS/NZS 4836 clause 3.2
3.2.1

All electrical conductors and parts including neutral and earthing conductors shall be treated as energized until proven de-energized

- (a) positively identified the relevant electrical equipment and conductors, all of their energy sources and the isolation points (clause 3.2.2)
- (b) Isolated electrical equipment and conductors from all energy sources (clause 3.2.3)

- (c) Secured the isolation (clause 3.2.4)
- (d) Discharged where necessary, any stored energy eg capacitors (3.9.2)
- (e) Provided the de-energization of all relevant electrical equipment and capacitors (3.2.5)
- (f) Identified the limits of the safe area of work (3.2.7)

SAFE RESTARTING SECTION 4) AS/NZS 4836

- (a) All relevant persons shall be notified that testing is about to commence (or) supply is about to be restored.
- (b) A visual inspection shall be conducted to ensure that all tools surplus material and wastes have been removed and the worksite has been reinstated.
- (c) visual inspection and tests required by AS/NZS shall be carried out.
- (d) Applicable work permits shall be cancelled.
- (e) Applicable personal tags and locks shall be removed.
- (f) Re-energizing as required by phase rotation are carried out.
- (g) Functional testing as required eg phase rotation are carried out
- (h) confirmation that all guards and covers are reinstated ~~is~~ is obtained.

Falling from height D/H use fall protection gear

PV Panel wiring short circuit D/H Test insulation resistance

Open circuit electrical shock D/H Test insulation resistance

Battery Acid injury D/H use glove, eye protection

Exposed terminals D/H Enclosed the exposed terminals

Live electrical terminals D/H ~~Test~~ Testing & Tagging

Environmental conditions - Items

- 1.1 Alternative supply equipment is suitably ventilated ✓
- 1.2 Alternative supply equipment is suitably rated for ambient temperature and humidity ✓
- 1.3 No external heat sources are present that may cause hazardous temperature rise ✓
- 1.4 Access and egress from the area is unobstructed ✓
- 2. Identification and labelling Item

- 2.1 system shutdown and startup procedures documented and available ✓
- 2.2 All required signage, labelling and markings are installed ✓
- 2.3 Shut down and start up procedures are consistent with diagrams and labelling ✓
- 3. control and protection - Item

- 3.1 All required isolation devices are installed and are operating correctly ✓
- 3.2 All required controls are installed correctly ✓
- 3.3 All required protection devices ~~are~~ and shrouds are installed correctly ✓
- 3.4 All required monitoring and alarms are installed correctly ✓

4. System Equipment (Items)

- 4.1 All terminations are suitably tight ✓
- 4.2 All system equipment is free from damage ✓
- 4.3 All system equipment is free from excessive dust, dirt and debris

5. System parameters (Items)

- 5.1 charger settings are correct and suitable for the required functionality
- 5.2 Inverter settings are correct and suitable for the required functionality

Alternative supply - operating voltages

Terminal	Test Results (V)	volt correct
Energy source output terminal	24.5V	✓
Battery bank terminal	28V	✓
Battery charger terminal	28V	✓
Inverter dc terminal	28V	✓
Inverter ac terminal	240V	✓

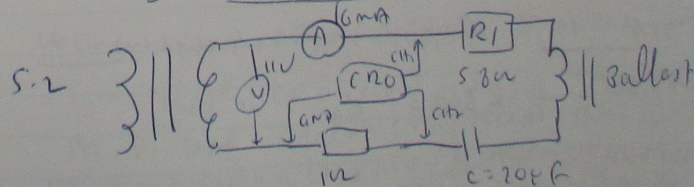
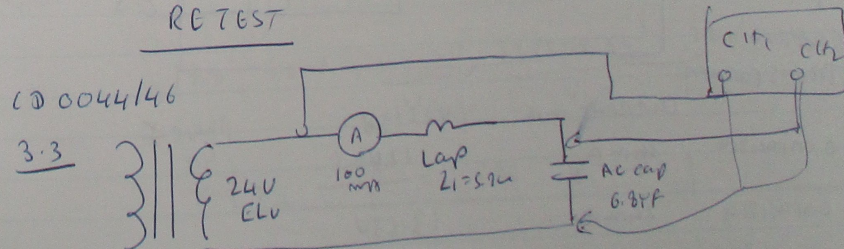
3 General Hazards noted by PV array

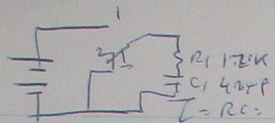
- 1/ The system may remain live between panels and isolation point
- 2/ Risk of fire
- 3/ Electrical spark occurs at dc/ac isolation switches

RISU noted by Automatic change over system

Modern Automatic Transfer switches are packed with sensitive electronics that are susceptible to damage. It may occasionally respond to false signals.

RETEST





Time to charge fully

$I = SRC = t = SRC = 57.6 \times 5 = 288$

Edw address
 EL008 4.1, 1.2, 4.2.1, 4.2.2, 3.3.2/2.3
 address
 EL010 1.2, 2.3, 3.2
 10/10/22 1.2 EL008 1.2.1, 1.2.2, 2.1, 2.2, 4.3, 5.2, 6.1, 6.2, 3.2
 11/10/22

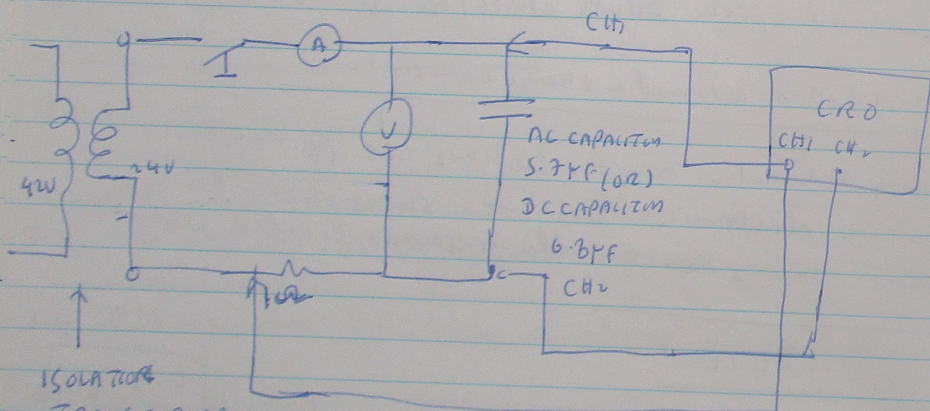
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RETEST WITH AC CAPACITOR

3.3, 5.2, 6.5

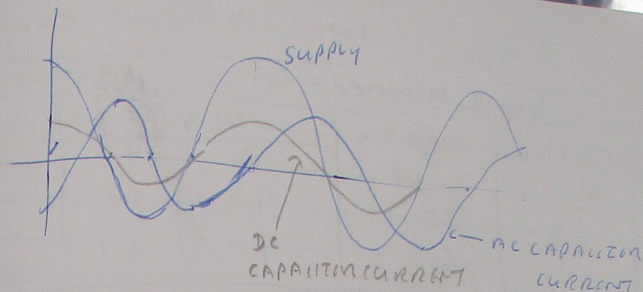
3.3 CAPACITANCE IN AC CIRCUIT



	CURRENT mA	Voltage	Phase ϕ
DC CAPACITAN	34 mA	12V	90
AC CAPACITAN	24 mA	13.53V	

CRO READING $d = 1$ division $T = 4$ division

$d = d/T \times 360 = \frac{1}{4} \times 360 = 90$



DC CAPACITAN

$Z = X_C = \frac{V}{I} = \frac{12}{34 \times 10^{-3}} = 352.9 \Omega$

AC CAPACITAN

$X_C = \frac{V}{I} = \frac{13.53}{24 \times 10^{-3}} = 562.91 \Omega$

$X_C = \frac{1}{2\pi f C}$

DC CAPACITAN $X_C = \frac{1}{2 \times 3.1416 \times 50 \times 6.8 \times 10^{-6}} = 462 \Omega$

AC CAPACITAN $X_C = \frac{1}{2 \times 3.1416 \times 50 \times 5.7 \times 10^{-6}} = 552 \Omega$

AC CAPACITAN GIVE MORE ACCURATE RESULT.

$S-Z$
 $X_C = \frac{1}{2\pi f C} = \frac{1}{2 \times 3.1416 \times 50 \times 55 \times 10^{-6}} = 57.9 \Omega$

R & C Series circuit
 $Z = \sqrt{1^2 + (343 - 57.9)^2} = \sqrt{1^2 + 285.1^2} = 285 \Omega$

$13.8, 38 \text{ mA}, \frac{0.032V}{V_R}, \frac{32 \times 57.9 \times 10^{-3}}{V_C}, 22V, V_L = 13V$

$\tan \phi = \frac{285}{1} = 285 \quad \phi = 89.7^\circ$

Warning, overvoltage in supply & m use only 42/240V supply, CRO ground and circuit ground conduct m, p use isolation transformer, overvoltage danger circuit m & check voltage rated & ratio of class series Electrolytic Cap: can be damaged by wrong polarity measure m & check capacitor type with test

Table 1 Measured valsp

CAPACITOR TYPE	RESISTOR Ω	CAPACITANCE μF	INDUCTANCE	
			Ω	μH
DC	5.8	20	9	1.1
AC	1	55	9	1.1

Table 2 calculated Reactance & Impedance

CAPACITOR TYPE	INDUCTIVE			CAPACITIVE	CIRCUIT	
	X_L	Z_L	Q_L		Z	ϕ
DC	342.88	343	88.4	159	159	90
AC	342.88	343	88.4	57.9	285	89.7

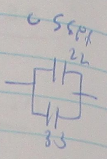


Table 3 calculated voltage & current

CAPACITOR TYPE	Supply voltage	current	Resistor voltage	Capacitor voltage	Inductor voltage
AC	13.8	38 mA	0.038V	2.2	13

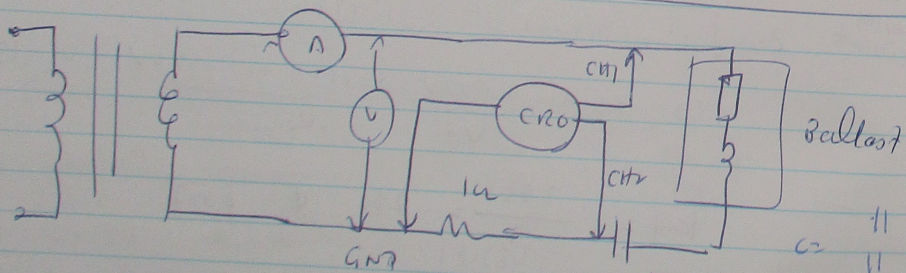
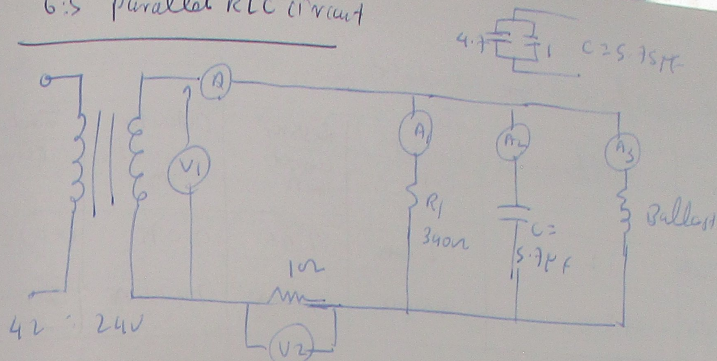


Table 4 Measured circuit parameters

CAPACITOR TYPE	Supply voltage	current	Resistor voltage	Capacitor voltage	Inductor voltage	Phase ϕ
AC	13.21	38 mA	0.038	4.27	17.74	89.4

6:5 parallel RLC circuit



2.1.1 circuit component

CAPACITOR TYPE	RESISTOR (R)	CAPACITANCE C	INDUCTANCE - Ballast	
			R	L
DC capacitor	5.8 Ohm	20 uF	9 Ohm	1.09 uH
AC capacitor	340 Ohm	5.7 uF	9 Ohm	1.09 uH

CAPACITOR TYPE	INDUCTIVE			CAPACITIVE	CIRCUIT	
	X_L	Z_L	Q_L		Z	ϕ
DC CAP.	479.9	480	88.9	159.23	5	1.31
AC CAP.	479.9	480	88.9	57.9	33.9	6.46

AC capacitor

$$X_C = \frac{1}{2\pi f C} = \frac{1}{2 \times 3.1416 \times 50 \times 5.7 \times 10^{-6}} = 57.9 \Omega$$

$$\frac{1}{Z_T} = \frac{1}{R} + \frac{1}{(X_L - X_C)} = \frac{1}{340} + \frac{1}{390}$$

$$\frac{1}{Z_T} = \frac{1}{R} + \frac{1}{jX_L} + \frac{1}{-jX_C} = \frac{1}{340} + \frac{1}{j479.9} - \frac{1}{j57.9}$$

$$= 2.94 \times 10^{-3} + (-j2.08 \times 10^{-3}) + j1.73 \times 10^{-3}$$

$$\frac{1}{Z} = 2.94 \times 10^{-3} + j(-2.08 \times 10^{-3} + 1.73 \times 10^{-3})$$

$$= \sqrt{(2.94)^2 + (-0.35)^2} \times 10^{-3}$$

$$= \sqrt{8.64 + 0.12} \times 10^{-3} = \sqrt{8.76} \times 10^{-3} = 2.96 \times 10^{-3}$$

$$Z = \frac{1}{2.96 \times 10^{-3}} = 337.8 \Omega$$

Use supply voltage calculate

Type of Capacitor	Supply voltage	Total current mA	Resistor current mA	Capacitor current mA	Inductor current mA
DC capacitor	12	2.0	2.06	0.075	0.025
AC capacitor	13.9	3.6 mA	35 mA	24.9 mA	29 mA

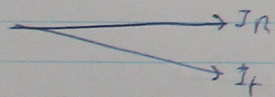
measured value

Branch current mA

Type of Capacitor	Supply voltage	Supply current mA	Resistor IR	Capacitor IC	Inductor IL	Phase angle
DC capacitor	12	1.50	8.5	36 mA	50 mA	10
AC capacitor	13.9	$\frac{0.041}{1} = 41 \text{ mA}$	34 mA	28 mA	30 mA	3.36

AC capacitor gives more accurate results between measured value and calculated value

$$\phi = \tan^{-1} \frac{30 - 28}{34} = 3.36$$



Branch current mA

Type of activity	Supply voltage volt	current mA	Resistor IR	Capacitor IC	Inductor IL	Phase Angle
Calculation	13.9	36 mA	35 mA	24.9 mA	29 mA	6.40
measuring	13.9	41 mA	34 mA	28 mA	30 mA	3.36

$$V_d = \frac{V_{CLZ}}{1000} = 0.336 = \frac{V_C 300}{1000} \quad I_L = \frac{V_C 300 \times 1000}{300 \times 12}$$

$$V_d = 0.336 \times 400$$

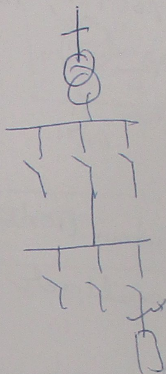
$$V_d \% = \frac{V_d \times 100}{400}$$

$$V_d = \frac{V_d \% \times 400}{100} = \frac{0.336 \times 400}{100} = 1.44$$

$$\text{Sum } V_d = \frac{0.92 \times 35 \times 160}{1000} = 5.152$$

$$V_C = \frac{V_d \times 1000}{300 \times 12} = \frac{1.44 \times 1000}{300 \times 12} = 0.320$$

$$\% V_d = \frac{5.152}{400} \times 100 = 1.22$$



$$\frac{(R_1 + R_x)^2}{2(R_1 + R_x)} = \frac{R_1 + R_x}{2}$$

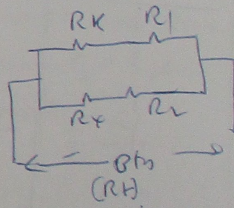
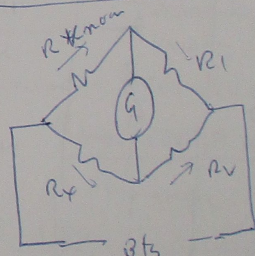
when bridge is balanced, the value is max.

$$R_t = \frac{R_1 + R_x}{2}$$

(or)

$$R_t = \frac{R_2 + R_x}{2}$$

$R_1 = R_x$ when ratio ratio = 1

$$\frac{R_1}{R_2} = 1 \rightarrow R_1 = R_2$$


$$R_t = \frac{(R_u + R_1)(R_x + R_2)}{R_u + R_1 + R_x + R_2}$$

$$= \frac{(R_u + R_1)(R_x + R_2)}{R_u + R_1 + R_x + R_2} = \frac{R_u R_x + R_1 R_2 + R_u R_2 + R_1 R_x}{R_u + R_x + R_2 R_1}$$

$$R_t = \frac{R_u R_x + R_1 R_2 + R_u R_2 + R_1 R_x}{R_u + R_x + R_2 R_1}$$

When $R_u = R_x \rightarrow R_t = \frac{R_x^2 + R_1 R_2 + R_x R_2 + R_1^2}{2 R_x + R_2 R_1} = \frac{R_x^2 + 2 R_x R_2 + R_2^2}{2(R_1 + R_2)}$

Practical - wheat stone Bridge Trainer

- STEP 1 - Setup the equipment
- STEP 2 - Set decade resistance value $1 \mu\Omega$
- STEP 3 - Then vary the ratio arm value 1
- STEP 4 - Press X_1 and X_2 to get the pointer position of galvanometer

If galvanometer indicates zero (middle) position, then calculate R_x as follows

$$R_{\text{unknown}} (\text{Decade resistance box value}) = \frac{R_1}{R_2}$$

$$\frac{1 \mu\Omega}{R_x} = 1 \quad \text{Thus } R_{\text{unknown}} (R_x) = 1 \mu\Omega$$

Take out R_{unknown} and measure it with multimeter = 999 Ω

Table 5.4

Ratio Arm	$\times 100$	$\times 1000$	Position of Galvanometer
1	0	2	Not at zero
1	0	3	Not at zero
1	0	4	Not at zero
1	3	1	Not at zero
0.01	0	1	Not at zero
10	0	1	Not at zero
1	0	1	At zero

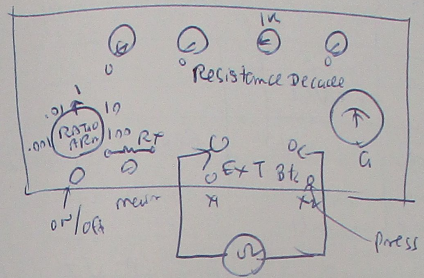
only at the balanced position, the galvanometer pointer indicates zero position and then the formula

$$R_{\text{unknown}} (\text{Decade Resistance box value}) = \frac{R_1}{R_2}$$

R_{unknown} can be utilized to calculate the unknown resistance R_x

5.2.1 Resistance measurement

wheat Stone Bridge Trainer



Ratio Arm	measured Resistance Value
0.001	307
0.01	300
1	411
10	393
100	300.6

- ① setup equipment
- ② set decade resistance value $1 \mu\Omega$
- ③ vary the ratio arm value 0.001, 0.01, 1, 10, 100, 1000 and the measured resistance shown on digital multimeter scale

At ratio arm value 1, the value of resistance is maximum, it means current flow will be minimum. At balanced condition, the current flow in

to galvanometer is minimum - for accurate measurement, it is zero.

The formula is
$$\frac{R_{\text{unknown}} (\text{Decade Resistor box})}{R_{\text{unknown}}} = \frac{R_1}{R_2}$$

$$\frac{1 \mu\Omega}{R_x} = 1 \rightarrow R_x = 1 \mu\Omega$$

Take out R_x , measure with multimeter = 999 Ω

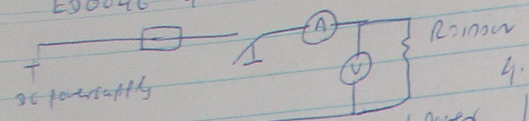
It is not actual wheatstone bridge, It is just a simulator to assist to understand the wheatstone bridge function.

It does not need supply.

- Ratio Arm - 1
- set $\times 1000$ - 1
- press X_1, X_2
- see galvanometer

then after $\times 100$ 1 \rightarrow 10
see what happen
alter $\times 1000$ 1 \rightarrow 10
what happen $R_x = 1 \mu\Omega$
at $\frac{1 \mu\Omega}{R_x} = 1$ Galv show 0

ES0046 4.2 Electrical Power



Setting	cont voltage	cont current mA	Power $P = VI$
Setting 1	10	95-100mA	1 watt
2	20	125-200mA	4 watt
3	30	245-300mA	9 watt

Replace R_1 with R_2 and test

Resistor	cont voltage	cont current mA	Power $P = VI$ watt
$R_1 = 100\Omega, 10W$	15V	140-160	1.46 - 2.56
$R_2 = 220\Omega, 10W$	15V	50-60	0.675 - 0.9W
$R_3 = 330\Omega, 5W$	15V	30-45	0.331 - 0.75

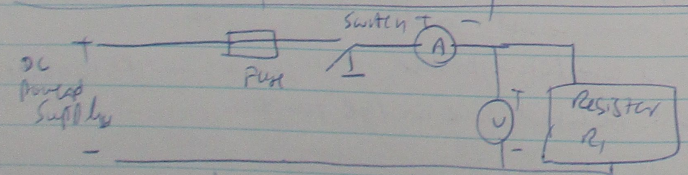
give voltage 3-3V

Resistor	Current (mA)	Volt (V)	Observation
$R_4 = 15\Omega, 10W$	0.2 - 0.23mA	3-3V	hot
$R_5 = 15\Omega, 5W$	0.2 - 0.23mA	3-3V	cold

R_1 - specified = 100Ω, R_1 measured 95-105Ω

Supply voltage 15V dc, record in Table 4.4

Voltage (V)	Current (mA)	Calc. Power
15	140mA	$P = VI$ $I^2 R$ $\frac{V^2}{R}$ 1.9-2.2 1.9-2.2 1.9-2.2



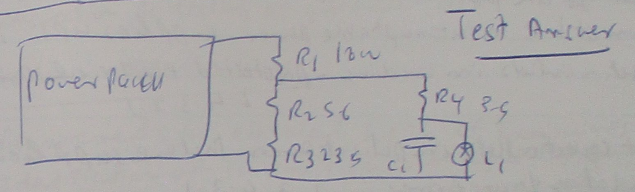
Current (mA)	Voltage (V)	watt = VI	meter	Actual
2	50	$2 \times 50 = 100W$	40%	40W
230mA	24	$0.23 \times 24 = 5.52$	55%	3.07W

Supply voltage doubled \rightarrow The power will increase 4 times
 doubled the value of capacitor - The power will decrease in half
 why resistors have a power rating

Resistors in an electric circuit have a limit to the amount of heat they can dissipate. This level of heat is expressed as power (in watts) and if this rating is exceeded the component will fail.

Does the practical give full proof of power equation
 $P = I^2 R$ and $P = \frac{V^2}{R}$

Yes, measured values are consistent with the equations
 $P = I^2 R$ and $\frac{V^2}{R}$



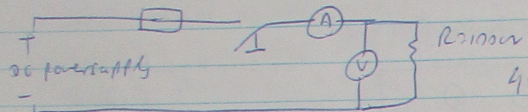
① R_1 short
 R_2 5.6
 R_3 23Ω
 $R_T = 5.6 + 23 = 28.6$

② R_1 open R_T d at

③ capacitor failure - shorting by insulation defect or open terminal due to overheat

④ Time delay $\tau = RC =$ charge R twice or charge C twice

E00046 4.2 Electrical power



Setting	cut voltage	cut current mA	Power $V = I \times R$	
Setting 1	10	95-100mA	1 watt	Replace R_1 with R_2, R_3
Setting 2	20	175-200mA	4 watt	Test
Setting 3	30	295-300mA	9 watt	

4.2 Resistor	cut voltage	cut current mA	power $P = V \times I$ watt
$R_1 = 100\Omega, 1W$	15V	140-160	1.46 - 2.56
$R_2 = 20\Omega, 10W$	15V	50-60	0.675 - 0.942
$R_3 = 35\Omega, 5W$	15V	30-45	0.351 - 0.75

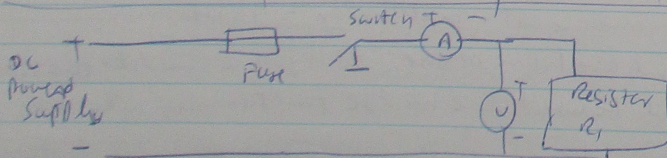
Give voltage 3.3V

4.3 Resistor	Current (mA)	Volt (V)	Observation
$R_1 = 100\Omega, 10W$	0.2 - 0.23mA	3.3V	hot
$R_2 = 15\Omega, 10W$	0.2 - 0.23mA	3.3V	cold

R_1 - specified = 100mA, R_1 measured 95-100mA

Supply voltage 15V dc, record in Table 4.4

4.4 Voltage V	Current (mA)	Calc. Power
15	140mA	$P = VI$ 1.9-2.2
		$I^2 R$ 1.9-2.2
		V^2/R 1.9-2.2



Current (amp)	Voltage (V)	watt = VI	meter	Actual
2	50	$2 \times 50 = 10W$	40%	40W
230mA	24	$0.23 \times 24 = 5.52$	55%	3.07 W

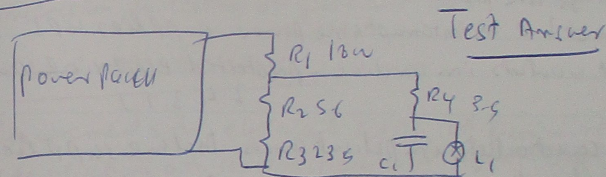
Supply voltage doubled \rightarrow The power will increase 4 times, doubled the value of capacitor - The power will decrease in half

Why resistors have a power rating

Resistors in an electric circuit have a limit to the amount of heat they can dissipate. This level of heat is expressed as power (in watts) and if this rating is exceeded the component will fail.

Does the practical give full proof of power equation $P = I^2 R$ and $P = V^2/R$

Yes, measured values are consistent with the equations $P = I^2 R$ and $\frac{V^2}{R}$



① R_1 short
 $R_T = 5.6 + 23.9 = 29.5\Omega$
 $R_2 \} 5.6$
 $R_3 \} 23.9$

② R_1 open $R_T = \infty$

③ capacitor failure - Shorting by simulation defect open terminal due to overheated

④ Time delay $\tau = RC =$ charge R, twice or charge C time

EL0012

3.1 Using Standards - Medical Treatment Areas

- Classification of body protected electrical area - 2 (2.4.1.1)
- Earthing in body protected electrical area - 3 (3.2)
- medical installations in residential homes - 5
- commissioning electrical installations in patient areas - 6
- Requirement of RCD in patient areas - 6
- Requirement for signage in a body-protected electrical area - 3
- Routine inspection & testing of protective earthing conductors in body protected area - 4.4.2.3
- Requirement for protection of L-V ac wiring systems against mechanical damage in patient areas - 6.3.2
- LPS protection of L-V uninterruptible power supplies UPS - 2.9.1
- Earthing of socket-outlets in cardiac-protected electrical area - 2.4.3.2.1

Identification of socket outlets in patient areas that are supplied from an isolation transformer - 2.7.4.3.1

- 1) 3 Australian standard - medical - 3900/3003/2500
- 2) Patient area - 2.2.1 AS3003 documentation outlining patient area locations and classification shall be provided by responsible organization/entity.

3) 6 Examples - body protected electrical area

- Anaesthetic bags, Audiometry, Blood collection, Chiropractic, Dental surgeries, Physiotherapy.

< Body protected electrical space is a patient care location that needs to undergo yearly routine inspection & testing.

every power point is protected by a safety switch. (imperative in any area where patients are being treated)

cardiac protected electrical area

measures micro shock is likely - (1) patient's intravascular device, 2) ECM monitoring.

- 1) Cardiac catheter laboratories
- 2) cardiac intensive care unit
- 3) coronary care unit
- 4) operations theatres used for cardiac surgery.

EL0012

3.2 Using standards - construction and demolition sites

AS3000 - applicable to specific electrical installation - section 7

AS3000:2012 Additional Requirement for electrical installation

7.6.2.1 - Electrical installations for construction and demolition sites shall comply with AS/NZS 3012.

AS 3012:2019 - Sections applicable to the sites on construction & demolition sites, AS 3012 sections

Installation of temporary switch boards - 2

Installation of temporary construction wiring - 2

Inspection and testing of temporary construction wiring - 3

Control and protection of construction wiring and equipment - 2

Verification of RCDs - 3

Inspection & testing of generator sets - 3

AS 3012 specific clause

Requirements for electrical supply of luminaires - 2.1.2

Identification of construction wiring - 2.5.4

Requirements for frame portable structures - 2.9

Requirement for documentation of periodic verification - 3.2

minimum IP rating of portable luminaires - 2.7.1

Definition of RCDP Inverter - 3.9

1/ Three Australian standards containing requirements for selection & installation of electrical wiring equipment

AS 3000 / 3012 / 3190

2/ Auxiliary socket outlet panel

AS 3012 1.4.7 A socket outlet assembly supplied by a fixed wire - dedicated final sub-circuit of construction wiring

3/ 3 types of construction (demolition sites covered by AS/NZS 3012: 2019)

① Building work

② The laying, lining (or) maintenance of pipes (or) cables

③ site offices.

3.3 Using standards - Relocable Installations

AS3000 - Specific Electrical Installation - Section 7

AS3000:2018 clause relating to additional requirements for electrical installations in caravans.

7.2.2.3 Electrical installations in transportable structures and vehicles including their site supplies shall comply with

AS/NZS 3001

AS3001 Section

- | | | |
|---|---|---|
| 1 | Protection of permanent wiring in caravans | 3 |
| 2 | Permanently connected appliances in caravans | 4 |
| 3 | Earthing of caravans | 3 |
| 4 | Inspection and Testing of electrical installation in caravans | 2 |
| 5 | Connection of caravan to a site supply using a supply lead | 5 |

AS3001 clause,

- 1/ Overcurrent protection of final sub-circuit in caravans 3.3.1.1 2-2-7.4
- 2/ minimum size of cables used in caravan wiring system 3.4-1
- 3/ parts of a caravan that are required to be earthed 3.5.1.2
- 4/ conductors permitted for use as equipotential bonding conductors 3.5.2
- 5/ Required IP rating of socket outlets installed on exterior of caravan 3.6.3.4
- 6/ Requirements for the control of a permanently connected electric cooker in a caravan 3.7-1

AS standards - Selection/Wiring in Caravan - AS 3001, 3002, 3012

Caravan AS3001 1.4.5 - A trailer designed to be towed by a road vehicle and often used for living and accommodation or a self-propelled vehicle (motor home) providing similar features to those of a caravan.

Transportable structures

- 1/ Relocable home
- 2/ site office
- 3/ display units not intended for accommodation.
- 4/ vending vans and trailers

3.4 Using standards - Caravan Parks

→ ALSO

AS/NZS 3001 Section

- 1/ Caravan supply arrangements from socket outlet in caravan parks - 4
- 2/ calculation of maximum demand for caravan park installation APPENDIX 'A'
- 3/ generator supply for caravan parks - 2
- 4/ Inspection and Testing of electrical installations in caravan parks - 3
- 5/ Provision of instructions for connection of caravans to caravan park supplies - 5

AS/NZS 3001

- 1/ Requirement of earthing of site supplies - 3-5
- 2/ Requirements for weather proofing of service pillars in caravan parks - 2-2-6.1 / 2-2-8.3
- 3/ minimum depth of cover for underground wiring system - 2-2-2
- 4/ Inspection and Testing of electrical installations in caravan parks - 3
- 5/ Provision of instructions for connection of caravans to caravan park supplies - 5
- 4/ Definition of Amenities - 1-4.1
- 5/ minimum rating for a socket outlet intended to supply a caravan 2-2-8.3

Aust. Std: Selection and installation of electrical wiring - Caravan AS3001, 3002, 3012

Service pillar 1.4.9 - A specialized switchboard together with its supporting structure. The switchboard contains one or more socket-outlets for the purpose of supplying power to transportable structures

Two camping areas not covered by 3001

- Transportable structures such as homes
- Vehicles that rendered immobile

3.5 Using standards marinas & Boats

Installation marina AS3002 Section 7
7.8.2.4 - Electrical installations in marinas and recreational boats shall comply with AS/NZS 3004.

- 1/ definition - 1 (AS3004 section) (AS3004:1:2014)
- 2/ low voltage switch boards for the supply of boats (2)
- 3/ use of isolation transformers in marinas - (2)
- 4/ methods of connections for boats - 3
- 5/ minimization of galvanic corrosion - 1

3004:1:2014 clause

- 1/ maximum number of socket-outlets permitted on a single service pillar - 2.8
- 2/ Requirements for bonding of metallic pipework in marinas - 3.6
- 3/ Types of supply leads permitted for the connection of recreational boats to the marina electrical installation - 4.2
- 4/ Requirements for periodic testing of RCDs - 2.6
- 5/ Wiring systems permitted for use in marina installations - 2.1

3004:2:2014 section

- 1/ definition - 1
- 2/ selection of cables for marine environment - 6
- 3/ cable support and protection on boats - 7
- 4/ Requirements for basic protection in low voltage ac installation on boats - 4
- 5/ shore connection arrangements - 3

3004:2:2014 clause

- 1/ definition of boat earth - 6.3
- 2/ Requirement for dc switch boards on boats - 3.1 / 3.6
- 3/ Protection by the use of class II equipment - 4.5
- 4/ maximum insulation resistance for lighting or power circuit on boats
- 5/ Additional Lithium battery installations on boats - 2.9 + 2.10

AS3004 + AS3002 + AS3082 (Safety criteria for elect. eqpt design)

- Safety voltage Sourceless - 1.4.12B
- Essential services on board boats
- Engine Drive System + Accessories
- 2/ Electrical system
- 3/ Ventilation + Air-con
- 4/ Navigational equipments

3.6 Using standards - Shows and Carnivals

Show / carnival AS3002 Section 4

7.8.2.5 Electrical installations in shows and carnivals shall comply with AS/NZS 3002.

AS3002/Section

- 1/ definitions - 1
- 2/ Permanent L-V switch boards on shows and carnival sites - 2
- 3/ Supplying shows and carnivals from an inverter system - 3
- 4/ carnival festoon lighting - 4
- 5/ carnival rides - 6
- 6/ cables used for temporary wiring of electrical equipment - 4

AS3002 clause

- 1/ minimum depth of cover for underground wiring systems - 2.1
- 2/ Selection of cables for temporary distribution systems - 4.2
- 3/ Types of inverters permitted for use on shows and carnival sites - 3.3
- 4/ Identification of switch boards - 2.4
- 5/ Testing RCD - 3.4
- 6/ over current protection of connection facilities - 2.4

Australian standards for shows and carnival wiring

AS3000, AS3002, AS3005 (Tents)

Definition of site

AS3002, 1.1

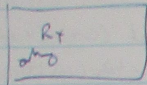
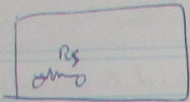
The supply of electricity at low voltage by wiring systems to power consuming devices used for accommodation, entertainment or display purpose within concessions, tents, living quarters and other structures.

max. duration of event covered by AS3002

4 weeks.

3 real world examples of events covered by AS/NZS 3002:2008

- Shows
- carnivals
- Exhibitions.

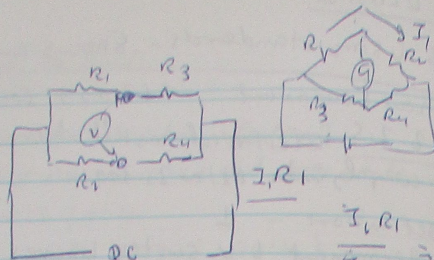


Ratio Arm

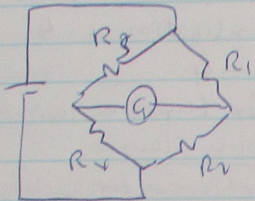
$$\frac{R_s}{R_x} = \frac{1}{10} \text{ to}$$

$$\frac{R_s}{R_x} = \frac{1}{100}$$

$$R_x = 10$$



$$\frac{I_1 R_1}{I_2 R_3} = \frac{I_1 R_2}{I_2}$$



Ratio Arm

$$\frac{R_s}{R_x} = \frac{R_1}{R_2}$$

$$\frac{1K}{10} = \frac{10}{10}$$

Set Ratio Arm = 1

Set x1000 → 1

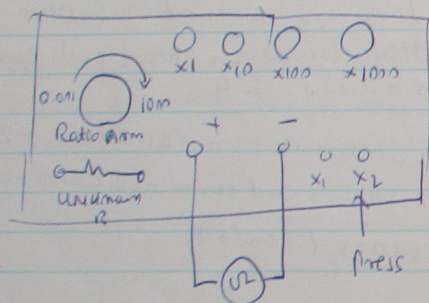
Press x1 x2

Set get meter

then Alter

x100 → 1 → 10

to meter.



Get $R_s = 1000$

$$\text{Ratio Arm} = \frac{1000}{100} = 10$$

$$100 = 389.7$$

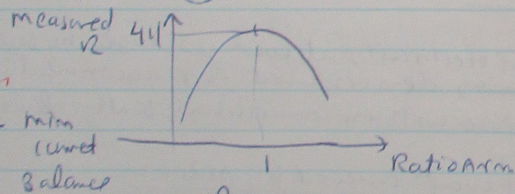
$$10 = 39.3$$

$$1 = 4.11$$

$$0.1 = 3.94$$

$$0.01 = 3.84$$

$$0.001 = 3.87$$



$$\frac{R_s}{R_x} = \text{Ratio Arm} = \frac{R_1}{R_2}$$

$$\frac{1000}{R_x} = 1 \Rightarrow R_x = 1000$$

measure in known Resistor = 0.9992 = 1000

You had to adjust decade Resistor

This is not actual wheel stone bridge just trainer but you can know he demonstrated wheel stone bridge

NSI ncc Requirements affecting electrical installation - Fire resistance, Emergency lighting exit signage, lighting and ventilation - Emergency efficiency.

EL0012 Apply Building codes and Heritage requirements

1.1 Apply Building Code Requirements

debris injuries DTH House Keeping / cut by sharp edge DTH
 use safety gear, Eye injury DTH use safety gear.
 wall socket outlet installation on fire rated wall

2.1.3 Wall base material - concrete, concrete block, reinforced concrete
 with 2 to 4 hours of fire ratings

method of installation - fire barrier leading with specified clearance
 wiring Rules / NCC Ref - NS 3000:2018 Clause 4.2.2.6 + 3.9.4.3

https://ncc.nsw.gov.au Section Fire resistance C.3.10

2.2.3 Install wiring in Building Structure

wiring system - wiring system shall be of a type that is capable of
 maintaining supply to equipment when exposed to fire or
 mechanical damage.

method of installation Install cables in steel conduit. NS 3000:2018

Flame retardant cable NS 2122, WS 52
 wiring Rules AS 3000:2018 Clause 7.2.72.1 (a) 2hr material

2.3 maintain Fire barrier

method of reinstating fire ratings - Utilize intumescent coating
 paints to achieve 2hr ratings | FRL - Fire Resistance Level (7.2.1.2, 7.2.4c)
 wiring Rules / NCC Ref - NCC Specification C.1.1 & section C Fire
 Resistant.

01 NCC - Electrical installation in a residential house → NCC vol 2

02 Electrical Installation in shopping centre class 1/17 - NCC vol 1
 NCC 2 - class 1 + 10a/b (NCC 1 - (2 → 9) NCC vol 3 - drainage/plumbing

03 maintenance of Fire barrier 3.9.4.3

AS 3000:2008 (3.9.4.3) The risk of spread of fire shall be
 minimized by selection of appropriate material in installation.
 wiring system shall be installed so that general building structure
 performance of fire safety are not reduced.

04 3.9.4.3 (AS 3000) - The opening shall be close fitting to the wiring
 system and at least 30mm from any service opening in the CSA
 of opening shall not be greater than 30mm.

E20012

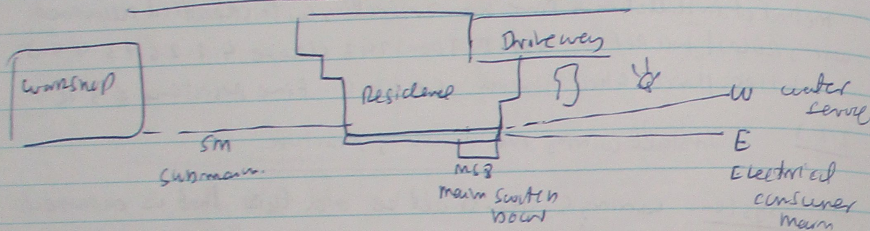
3.1 using Standards - medical treatment Area

AS/NZS 3000-2018 Section 7

AS/NZS 3000 Clause 7.8.2.2

Requirement - Electrical Installation in Electromedical Treatment Area shall comply with AS/NZS 3000

Cluster Skills Test Phase 2



Residence

Qty	Type
✓ 2	lighting points
✓ 2	40w 230V Exh fan
✓ 27	10A 230V double socket outlet
✓ 5	10A, 230A single socket outlet
1	15A, 230A single socket outlet
1	11kW 230V upright stove
1	12-Skw, 400V 3φ Inst-water heater
1	230V reverse cycle Aircon (12.4A max)

Workshop

Qty	Type
✓ 9	lighting points
✓ 1	80w, 230V Exh fan
✓ 7	10A 230V double socket outlet
✓ 4	10A 230V single socket outlet
1	15A 230V single outlet
1	3-Skw 400V wood Lake
1	2.4kW 230V Airw luminaire

Residence + Workshop

Load	Load group	Calculation	A	B	C
20 lighting points	(C1)	20pt - 3A Add 20pt = 2A 5A		SA	
2 x 40w 230V Exh fan	(A1)				
27 10A double socket	(C1)	27 x 2 = 54			
5 x 10A single socket	(B1)	5 x 1 = 5 5A			
10 x (10A double socket outlet)		2 x 10 = 20 (10A for 1-20m)			10
10 (10A double socket outlet)		2 x 10 = 20			10
7 (10A double socket outlet) + 5 x 10A single outlet		7 x 2 + 5 = 19			10
1 x 15A 230V single socket outlet	(B1ii)	10A			10
1 x 11kW 230V upright stove	(E)	50% connected load $\frac{11 \times 1000}{230} \times 0.5 = 23.9$		23.9	
1 x 12-Skw 400V 3φ Inst-water heater	(E)	$\frac{33.3 \times 12.5 \times 10^3}{1.7321 \times 400} \times 0.333 =$		6	6
230V Reverse cycle Aircon	(C)	7.57 12.4A x 0.75 = 9.3			13.8
				29.9	34.0
					36

Maximum demand = 36A. for residence.

Load	Load Group	Calculation	A	B	C
RES			29.9	34.8	36
8 lighting pt. 80W 230V Ech fan	workshop All 8 light + 1 ECh fan = 9 pt	8 light + 1 ECh fan 9 pt ⇒			
7 x 10A 230V double socket outlet + 4 x 10A 230V single socket	B(i)	7 x 2 = 14 pt + 4 18	10 (42.1)	(34.0)	(36)
15A 230V single socket	B(ii)	10A	10A	(44.0)	(36)
1 x 3-wire knob and tube	C2 (d)	$\frac{3 \times 5 \times 10^3}{1.732 \times 230} = 5.05$	S	S	35A
2 x 4kW 230V air comp.		$\frac{2.4 \times 10^3}{230} = 10.4$			10.4
		TOTAL SM	18	15	15
		TOTAL	47.9	49.0	51.4

current carrying capacity of consumer main
3 core cable enclosed UG.
Installation condition UG
conduit, use X90

maximum demand = 51.4 for Residence +
maximum demand = 18 for workshop
maximum demand 36 for Residence.

Table 3(4) UG wiring Enclosure one 3 core cable
Element 4, → Table 13/14/ col 25-27
use V90 → Table 14 col 25 15 col 15 demand
51.4A - (3A) → 10mm² Act = 1

Vd Table 42 multicore UG
V90 → 10mm² → 405
Vd γ = $\frac{1.66}{415} \times \frac{405}{1000} = 0.32\%$ ✓ = 4.16

Length = 20m
Vd > $\frac{Vd \times I}{1000} = \frac{4.05 \times 51.4}{1000}$

submain > 18A max. demand Table 3(4) X90 Table 14 col 15
Vd = Table 42 multicore 2.5mm² → 16.4
 $Vd = \frac{Vd \times I}{1000} = \frac{16.4 \times 55 \times 18}{1000} = 16.25V$
 $\frac{16.25}{415} \times 1000 = 3.9\%$

4mm² Vd = $\frac{10.2 \times 55 \times 18}{1000} = 10.09 = \frac{10.09}{415} \times 1000 = 2.43\%$
6mm² Vd = $\frac{6.6 \times 55 \times 18}{1000} = 6.72 = \frac{6.72 \times 1000}{415} = 1.61\%$
10mm² Vd = $\frac{4.05 \times 55 \times 18}{1000} = 4.0096 = \frac{4.0096 \times 1000}{415} = 0.96\%$
Choose 10mm² X90 cable.

consumer main min. cable size 10mm ²	CURRENT CARRYING CAPACITY TABLE COLUMN 14 25	RATING / ORATING TABLE COL 22 4
voltage drop cable size 10mm ²	cut load 51.4	Route length 8
	volt. drop 1.66	AS 3000 Table 42 42 8

Submain min cable size 2.5mm ² load	current carrying capacity TABLE COL 14 25	Rating Table COL 22 4
voltage drop cable size 10mm ²	cut load 18	Route length 55
	volt. drop 4.0096	AS 3000 Table 42 42 8

Final subcircuit V90 circular 4 core TPS V90
15mm clipped to timber ceiling joist, imbed ed.
12.5kW, 400V 3φ Instantaneous water heater V90 11mm
 $I = \frac{12.5 \times 10^3}{\sqrt{3} \times 400} = 18.04A$ max demand = 33.3% = 6A
Table C9. - connected load

Earth fault loop impedance? Total length = 55 + 8 = 63m.
AC RESISTANCE
cables = Active = 10mm² (55 + 8) =
90°C
10mm² → 2.332 (40m) → $\frac{2.332 \times 63}{1000} = 0.1469$
Table 35
3000
ACTIVE Earth Table 35/3000
10mm² 4mm² → 5.89uΩ
5.89uΩ/1mm = 0.37
Total React fault loop Earth cable size = 3mm →
= 0.1469 + 0.37 = 0.515uΩ Table 5-1